

M99M.3

We use $u(r, \phi)$ to denote the deformation of the drum (the membrane). The force \vec{F} on a small fraction of the drum at (r, ϕ) is

$$\delta\vec{F} = \delta m \vec{g} + \vec{P} \quad (1)$$

where \vec{P} is the force from the tension of the drum.

$$\delta F_{\perp} = \delta m g + P_{\perp} \quad (2)$$

$$\delta F_{\parallel} = P_{\parallel} \quad (3)$$

where \perp denotes the vertical direction, and \parallel denotes the horizontal direction.

Consider the tension on a small fraction of the drum with vertice at

$(x, y), (x + \delta x, y), (x + \delta x, y + \delta y), (x, y + \delta y)$, where $x = r \cos \phi, y = r \sin \phi$. Assume the displacement of this piece is $u(x, y)$. The angle between $u(x, y)$ and (x, y) plane has a projection $\theta = \arctan\left(\frac{\partial u}{\partial x}\right) \sim \frac{\partial u}{\partial x}$ on the (y, z) plane.

Therefore we should have the tension on the x direction and on the vertical direction as:

$$P_{\perp} = (\tau \delta y \sin \theta)_{x+\delta x} - (\tau \delta y \sin \theta)_x \sim (\tau \delta y \theta)_{x+\delta x} - (\tau \delta y \theta)_x = (\tau \delta y \theta)_{x+\delta x} - (\tau \delta y \theta)_x$$

$$P_{\parallel} = (\tau \delta y \cos \theta)_{x+\delta x} - (\tau \delta y \cos \theta)_x \sim (\tau \delta y (-\frac{1}{2}) \theta^2)_{x+\delta x} - (\tau \delta y (-\frac{1}{2}) \theta^2)_x$$

consider $\theta = \frac{\partial u}{\partial x}$, and the same picture for the y direction (Assume the projection of the intersection angle on x, z plane is $\theta' = \frac{\partial u}{\partial y}$), we can get:

$$\begin{aligned}
P_{\perp} &= \tau\delta y \left[\left(\frac{\partial u}{\partial x} \right)_{x+\delta x} - \left(\frac{\partial u}{\partial x} \right)_x \right] + \tau\delta x \left[\left(\frac{\partial u}{\partial y} \right)_{y+\delta y} - \left(\frac{\partial u}{\partial y} \right)_y \right] \\
&= \tau\delta x\delta y \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right] \\
&= \tau\delta A \nabla^2 u \quad (4)
\end{aligned}$$

$$P_{\parallel} = \tau\delta y \frac{1}{2} \left[- \left(\frac{\partial u}{\partial x} \right)_{x+\delta x}^2 + \left(\frac{\partial u}{\partial x} \right)_x^2 \right] + \tau\delta x \frac{1}{2} \left[- \left(\frac{\partial u}{\partial y} \right)_{y+\delta y}^2 + \left(\frac{\partial u}{\partial y} \right)_y^2 \right] \quad (5)$$

where $\delta A = \delta x\delta y$ is the area of the small fraction of the drum.

Since we consider small deformation, $\frac{\partial u}{\partial x_i}$ is considered small, that is, $\frac{\partial u}{\partial x_i} \ll 1$, therefore, $P_{\parallel} \ll P_{\perp}$, so we consider only the vertical force on the drum, getting:

$$\delta F = \delta m g + \tau\delta A \nabla^2 u \quad (6)$$

$$\Rightarrow \delta m \frac{\partial^2 u}{\partial t^2} = \delta F = \delta m g + \tau\delta A \nabla^2 u \quad (7)$$

$$\Rightarrow \frac{\partial^2 u}{\partial t^2} - \frac{\tau}{\rho} \nabla^2 u = g \quad (8)$$

where $\rho = \frac{\delta m}{\delta A}$ is mass per unit area.

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(a) The center sag below the rim is displacement at the center $u|_{r=0}$.

Equilibrium state, so we have

$$\frac{\partial u}{\partial t} = 0. \quad (9)$$

From the azimuthal symmetry we have

$$\frac{\partial u}{\partial \phi} = 0. \quad (10)$$

We also have the edge of the drum is the level of the rim, and the center does not sag to infinitely low level:

$$u|_{r=R} = 0 \quad (11)$$

$$u|_{r=0} = \text{finite} \quad (12)$$

from (8), (9), (10) and the form of u in cylindrical geometry we have:

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u}{\partial r} \right) + \frac{\rho g}{\tau} = 0 \quad (13)$$

$$\Rightarrow u = A_1 r^2 + B_1 \ln r + C_1 \quad (14)$$

From (13) we have $A_1 = -\rho g/4\tau$. From (12) we have $B_1 = 0$. From (11) we have $C_1 = \frac{\rho g}{4\tau} R^2$.

Therefore we have

$$u = -\frac{\rho g}{4\tau} r^2 + \frac{\rho g}{4\tau} R^2 \quad (15)$$

$$u|_{r=0} = \frac{\rho g}{4\tau} R^2 \quad (16)$$

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(b) Assume $u = R(r)\Phi(\phi)T(t)$. From (8) and $g = 0$, we have

$$\frac{T''}{T} - \frac{\tau}{\rho} \left[\frac{(rR')'}{rR} + \frac{\Phi''}{r^2\Phi} \right] = 0 \quad (17)$$

$$R(r=0) = \text{finite} \quad (18)$$

$$R(r=R) = 0 \quad (19)$$

$$\Phi(0) = \Phi(2\pi) \quad (20)$$

$$\Phi'(0) = \Phi'(2\pi) \quad (21)$$

where $X(x)' = \frac{dX}{dx}$ denotes first order derivative, and $X(x)'' = \frac{d^2X}{dx^2}$ denotes second order derivative.

From (17) we have:

$$T'' + \omega^2 T = 0 \Rightarrow T = A_\omega e^{i\omega t} + B_\omega e^{-i\omega t} \quad (22)$$

$$\Phi'' + m^2 \Phi = 0 \Rightarrow \Phi_m = \cos(m\phi) + C_m \sin(m\phi) \quad (23)$$

$$(20) \& (21) \Rightarrow m \in \mathbb{Z}$$

$$\frac{(rR'_m)'}{(rR_m)} + \left(\frac{\omega_i^2 \rho}{\tau} - \frac{m^2}{r^2} \right) = 0 \quad (24)$$

$$\Rightarrow R_m = J_m(kr) + D_m N_m(kr) \quad (25)$$

where $A, B, C \& D$ are parameters determined by the initial condition. $k^2 = \omega^2 \rho / \tau$.

From (18), we get $D_m = 0$ for any m .

From (19), we get

$$J_m(kR) = 0 \Rightarrow \quad (26)$$

$$k = k_{im} = \frac{\mu_{im}}{R} \Rightarrow \omega_{im} = \frac{\mu_{im}}{R} \sqrt{\frac{\tau}{\rho}} \quad (27)$$

where μ_{im} is the i^{th} 0 point of the m^{th} order Bessel function $J_m(x)$, s.t. For $m = 0, 1, 2, \dots$, $J_m(\mu_{im}) = 0$, ($i = 0, 1, 2, \dots$).

In the problem, the smallest zero point $\mu_{00} = 0.766\pi$ is given. From (27) we have

$$\omega_{00} = 0.766\pi \sqrt{\frac{\tau}{\rho R^2}} \quad (28)$$

Therefore the lowest vibrational frequency f would be

$$f = \omega_{00}/2\pi = 0.383 \sqrt{\frac{\tau}{\rho R^2}} \quad (29)$$

One thought on "M99M.3"



October 17, 2013 at 5:18 pm

Very good. I have no major comments.

Just two small ones:

- 1) in the first line of your solution you write $u(r, z, \phi)$, why do you include z ?
- 2) Equation (5) looks a bit suspicious. Even though the exact expression in (5) doesn't make any impact on your solution, it's better to reexamine it (and maybe provide some explanation?).