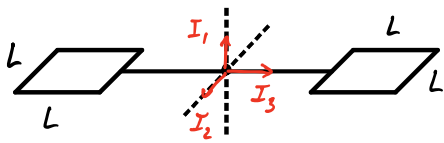


M18M.3 (Space Panels)

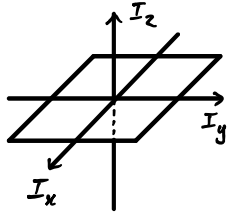
(a)



By \bar{e} symmetries of \bar{e} problem, it is clear \bar{e} principle axes are
 \bar{e} axis of \bar{e} beam, \bar{e} axis in \bar{e} plane of \bar{e} panels \perp to \bar{e} beam,
 \bar{e} \bar{e} axis \perp to \bar{e} plane of \bar{e} panels.

Visually, it looks like we have $I_3 < I_2 < I_1$, as shown above.

First, we will find \bar{e} moments of inertia of \bar{e} planar square panel through \bar{e} centre.



\perp axis thm: $I_z = I_x + I_y$

$$I_x = I_y = \frac{m}{L^2} \int_{-L/2}^{L/2} dx \int_{-L/2}^{L/2} dy y^2$$

$$= \frac{4m}{L^2} \int_0^{L/2} dx \int_0^{L/2} dy y^2$$

$$= \frac{4m}{L^2} \cdot \frac{L}{2} \cdot \frac{1}{3} \cdot \frac{L^3}{8}$$

$$= \frac{1}{12} mL^2 \implies I_z = \frac{1}{6} mL^2$$

Return³ to \bar{e} problem, we immediately see \bar{e} $I_3 = \frac{1}{6} mL^2$

For I_2 , we apply \bar{e} \parallel axis thm to I_x from before:

$$I_2 = 2 \cdot \left(I_x + m \cdot \frac{1}{2} (L+d)^2 \right)$$

$$= \frac{1}{6} mL^2 + mL^2 + 2mLd + md^2$$

$$= \frac{7}{6} mL^2 + md^2 + 2mLd$$

Similarly, for I_1 we apply \bar{e} \parallel axis thm to I_z :

$$I_1 = 2 \cdot \left(I_z + m \cdot \frac{1}{2} (L+d)^2 \right)$$

$$= \frac{1}{3} mL^2 + mL^2 + 2mLd + md^2$$

$$= \frac{4}{3} mL^2 + md^2 + 2mLd$$

From this, it's clear \bar{e} $I_3 < I_2 < I_1$, as required.

(b) For \bar{e} pseudogravity at \bar{e} centre of each panel to be $\frac{g}{6}$, we must have:

$$\vec{\omega} = \frac{g}{3(L+d)} \hat{z}, \text{ where } \bar{e} \hat{1}, \hat{2}, \hat{3} \text{ axes are } \bar{e} \text{ principal axes from before.}$$

$$\bar{e} \text{ Euler equat}^{\text{ns}} \text{ are derived as: } \left. \frac{d\vec{L}}{dt} \right|_{\text{inertial}} = \left. \frac{d\vec{L}}{dt} \right|_{\text{rot}} + \vec{\omega} \times \vec{L}$$

$$\begin{cases} \tau_1 = \frac{dL_1}{dt} + \omega_2 L_3 - \omega_3 L_2 = I_1 \dot{\omega}_1 + \omega_2 \omega_3 (I_3 - I_2) \\ \tau_2 = \frac{dL_2}{dt} + \omega_3 L_1 - \omega_1 L_3 = I_2 \dot{\omega}_2 + \omega_1 \omega_3 (I_1 - I_3) \\ \tau_3 = \frac{dL_3}{dt} + \omega_1 L_2 - \omega_2 L_1 = I_3 \dot{\omega}_3 + \omega_1 \omega_2 (I_2 - I_1) \end{cases} \xrightarrow{\vec{\tau} = 0} \begin{cases} I_1 \dot{\omega}_1 + \omega_2 \omega_3 (I_3 - I_2) = 0 \\ I_2 \dot{\omega}_2 + \omega_1 \omega_3 (I_1 - I_3) = 0 \\ I_3 \dot{\omega}_3 + \omega_1 \omega_2 (I_2 - I_1) = 0. \end{cases}$$

In this problem, we apply a small perturbat^o to \bar{e} rotat^o about I_2 . So, we can say:

$$\omega_2 \rightarrow \omega_2 - \epsilon$$

$$\omega_3 \rightarrow \epsilon \text{ (assume } \bar{e} \text{ perturbat}^{\text{o}} \text{ excites } I_3 \text{ rotat}^{\text{o}}).$$

$$\text{Differentiate } \bar{e} \text{ 3}^{\text{rd}} \text{ Euler equat}^{\text{ns}}: I_3 \ddot{\epsilon} + (I_2 - I_1)(\dot{\omega}_1 \omega_2 + \omega_1 \dot{\omega}_2) = 0$$

$$\text{Drop } \bar{e} \omega_1 \text{ term: } I_3 \ddot{\epsilon} = -(I_2 - I_1) \dot{\omega}_1 \omega_2$$

$$\text{Substitute } \omega_1 \text{ from } \bar{e} \text{ 1}^{\text{st}} \text{ equat}^{\text{ns}}: \ddot{\epsilon} = -\frac{1}{I_3} (I_2 - I_1) \omega_2^2 \omega_3 \frac{1}{I_1} (I_2 - I_3)$$

$$\approx \epsilon \cdot \frac{\omega_2^2}{I_1 I_3} (I_1 - I_2)(I_2 - I_3) \equiv \Omega^2 \epsilon, \quad \omega / \Omega^2 > 0.$$

$$\text{Thus, this is a grow}^2 \text{ perturbat}^{\text{o}}, \text{ w/ characteristic freq. } \Omega = \omega_2 \sqrt{(1 - \frac{I_2}{I_1})(\frac{I_2}{I_3} - 1)}$$

$$\implies \bar{e} \text{ characteristic time is } \tau \sim \frac{1}{\Omega} \text{ y.}$$