

## J11E.1 Solution

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a) luckily for me I remembered several things that were very helpful for this problem. Most importantly

$$\langle \vec{S} \rangle = \frac{1}{2} \vec{E} \times \vec{H}^*$$

Then, knowing your trusty wave solutions to Maxwell's equations in a coaxial cable (since  $k$  isn't specified in the problem let  $k = \omega/c$ ) you can solve for the time averaged Poynting vector

$$\begin{aligned}\vec{E} &= \frac{E_0}{s} e^{i(kz - \omega t)} \hat{s} \\ \vec{B} &= \frac{E_0}{sc} e^{i(kz - \omega t)} \hat{\phi} \\ \langle \vec{S} \rangle &= \frac{E_0^2}{2s^2 c \mu_0} \hat{z}\end{aligned}$$

then relate that to the time averaged power radiated via

$$\begin{aligned}\langle P \rangle &= \int \langle \vec{S} \rangle \cdot d\vec{A} \\ \langle P \rangle &= \int_0^{2\pi} \int_a^b \frac{E_0^2}{2s^2 c \mu_0} s ds d\phi \\ \langle P \rangle &= \frac{E_0^2 \pi}{2c \mu_0} \log(b/a)\end{aligned}$$

b) A good thing to memorize from Griffith's is the relation between the incident, reflected, and transmitted wave amplitudes

$$\begin{aligned}E_R &= \frac{1 - \beta}{1 + \beta} E_I \\ E_T &= \frac{2}{1 + \beta} E_I\end{aligned}$$

Where  $\beta = \frac{\mu_1 v_1}{\mu_2 v_2}$ . so for situations like this where  $\mu_1 \approx \mu_2$  (which is most materials by the way)  $\beta \approx \sqrt{\epsilon_r}$  where  $\epsilon_r = \frac{\epsilon}{\epsilon_0}$

$$\begin{aligned}\vec{E}_R &= \frac{E_0}{s} \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} e^{i(kz - \omega t)} \hat{s} \\ \vec{B}_R &= - \frac{E_0}{sc} \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} e^{i(kz - \omega t)} \hat{\phi}\end{aligned}$$

Where the negative on  $\vec{B}_R$  is from the flipping at the boundary. This is necessary since otherwise the poynting vector would still be propagating in the  $+\hat{z}$  direction

$$\begin{aligned}\vec{E}_T &= \frac{E_0}{s} \frac{2}{1 + \sqrt{\epsilon_r}} e^{i(kz - \omega t)} \hat{s} \\ \vec{B}_T &= \frac{E_0}{sc} \sqrt{\epsilon_r} \frac{2}{1 + \sqrt{\epsilon_r}} e^{i(kz - \omega t)} \hat{\phi}\end{aligned}$$

Note that the  $k$  in the transmitted wave functions are not the same as in the reflected since in the transmitted waves  $k = \omega\sqrt{\epsilon_r}/c$

c) To find the force per unit area all we need is the net radiation pressure from all these EM-waves. This is given by

$$\begin{aligned}P_{rad} &= \frac{|\langle \vec{S} \rangle|}{c} \\ P_{rad} &= \frac{|\langle \vec{S}_I \rangle|}{c} - \frac{|\langle \vec{S}_R \rangle|}{c} - \frac{|\langle \vec{S}_T \rangle|}{c} \\ P_{rad} &= \frac{E_0^2}{2s^2c^2\mu_0} - \frac{E_0^2}{2s^2c^2\mu_0} \left( \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} \right)^2 - \frac{E_0^2\sqrt{\epsilon_r}}{2s^2c^2\mu_0} \left( \frac{2}{1 + \sqrt{\epsilon_r}} \right)^2\end{aligned}$$

Some algebra yields the answer

$$\begin{aligned}P_{rad} &= \frac{E_0}{s^2c^2\mu_0} \left( \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} \right)^2 \\ \Rightarrow \vec{F}_{total} &= \int_0^{2\pi} \int_a^b \frac{E_0}{s^2c^2\mu_0} \left( \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} \right)^2 s ds d\phi \hat{z} \\ \vec{F}_{total} &= \frac{E_0}{c^2\mu_0} \left( \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} \right)^2 \log(b/a) \hat{z} \\ \vec{F}_{average} &= \frac{E_0}{\pi(b^2 - a^2)c^2\mu_0} \left( \frac{1 - \sqrt{\epsilon_r}}{1 + \sqrt{\epsilon_r}} \right)^2 \log(b/a) \hat{z}\end{aligned}$$